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a frequency range of 100 MHz to 10 GHz, and

a relative bandwidth bwr is not greater than 200% where the relative bandwidth bwr is obtained by extracting a frequency bandwidth between two frequencies at which the value of μ'' is 50% of the maximum μ''_{\max} and normalizing the frequency bandwidth at the center frequency thereof.

9. The wiring board according to claim 8, wherein X component of said magnetic loss material is at least one of C, B, Si, Al, Mg, Ti, Zn, Hf, Sr, Nb, Ta, and rare earth elements.

10. The wiring board according to claim 8, wherein, in said magnetic loss material, said M exists in a granular form dispersed in matrix of said X-Y compound.

11. The wiring board according to claim 8, wherein mean particle diameter of particles M having said granular form is within range of 1 nm to 40 nm.

12. The wiring board according to claim 8, wherein said magnetic loss material exhibits an anisotropic magnetic field H_k of 600 Oe (4.74×10^4 A/m) or less.

13. The wiring board according to claim 8, wherein said magnetic loss material is selected from $\text{Fe}_\alpha\text{-Al}_\beta\text{-O}_\gamma$ and $\text{Fe}_\alpha\text{-Si}_\beta\text{-O}_\gamma$.

14. The wiring board according to claim 8, wherein size of saturation magnetization in said magnetic loss material is within a range of 80% to 60% of saturation magnetization of a metal magnetic body consisting solely of M component.

15. The wiring board according to claim 8, wherein said magnetic loss material exhibits a DC electrical resistivity that is within a range of $100 \mu\Omega\cdot\text{cm}$ to $700 \mu\Omega\cdot\text{cm}$.

16. The wiring board according to claim 1, wherein said magnetic thin film is configured of a magnetic loss material having a composition represented

by M-X-Y, where M is at least one of Fe, Co, and Ni, X is at least one element other than M or Y, and Y is at least one of F, N, and O,

said magnetic loss material is a broad-band magnetic loss material in which maximum value μ''_{\max} of loss factor μ'' that is imaginary component in complex permeability characteristic of said magnetic loss material exists within a frequency range of 100 MHz to 10 GHz, and

a relative bandwidth bwr is not smaller than 150% where the relative bandwidth bwr is obtained by extracting a frequency bandwidth between two frequencies at which the value of μ'' is 50% of the maximum μ''_{\max} and normalizing the frequency bandwidth at the center frequency thereof.

17. The wiring board according to claim 16, wherein size of saturation magnetization of said magnetic loss material is within range of 60% to 35% of saturation magnetization of a metal magnetic body consisting solely of M component.

18. The wiring board according to claim 16, wherein said magnetic loss material exhibits a DC electrical resistivity having a value larger than 500 $\mu\Omega\cdot\text{cm}$.

19. A wiring board comprising:

a board of at least one layer comprising a conductor part; and magnetic thin films deployed at least on part of said board or said conductor part.

20. The wiring board according to claim 19, wherein said conductor part has a ground part that is either a ground surface or that comprises ground patterns deployed on one surface of said board, and entire surface of said ground part is covered with a magnetic thin film.

21. The wiring board according to claim 19, wherein said conductor part comprises at least one of ground patterns or conductor patterns deployed on one surface of said board, or comprises a ground surface deployed over

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frequencies at which the value of μ'' is 50% of the maximum μ''_{\max} and normalizing the frequency bandwidth at the center frequency thereof.

30. The wiring board according to claim 29, wherein size of saturation magnetization in said magnetic loss material is within a range of 60% to 35% of saturation magnetization of a metal magnetic body consisting solely of M component.

31. The wiring board according to claim 19, wherein said magnetic loss material exhibits a DC electrical resistivity having a value larger than $500 \mu\Omega\cdot\text{cm}$.

32. The wiring board according to claim 22, wherein said magnetic thin film is configured of a magnetic loss material having a composition represented by M-X-Y, where M is at least one of Fe, Co, and Ni, Y is at least one of F, N, and O, and X is at least one element other than M or Y,

said magnetic loss material is a narrow-band magnetic loss material in which maximum value μ''_{\max} of loss factor μ'' that is imaginary component in complex permeability of said magnetic loss material exists within a frequency range of 100 MHz to 10 GHz, and

a relative bandwidth bwr is not greater than 200% where the relative bandwidth bwr is obtained by extracting a frequency bandwidth between two frequencies at which the value of μ'' is 50% of the maximum μ''_{\max} and normalizing the frequency bandwidth at the center frequency thereof.

33. The wiring board according to claim 32, wherein size of saturation magnetization in said magnetic loss material is within a range of 80% to 60% of saturation magnetization of a metal magnetic body consisting solely of M component.

34. The wiring board according to claim 32, wherein said magnetic loss material exhibits a DC electrical resistivity that is within a range of $100 \mu\Omega\cdot\text{cm}$ to $700 \mu\Omega\cdot\text{cm}$.

35. The wiring board according to claim 32, wherein X component of said magnetic thin film is at least one of C, B, Si, Al, Mg, Ti, Zn, Hf, Sr, Nb, Ta, and rare earth elements.

36. The wiring board according to claim 32, wherein, in said magnetic loss material, said M exists in a granular form dispersed in matrix of said X-Y compound.

37. The wiring board according to claim 32, wherein mean particle diameter of particles M having said granular form is within range of 1 nm to 40 nm.

38. The wiring board according to claim 32, wherein said magnetic loss material exhibits an anisotropic magnetic field H_k of 600 Oe (5.34×10^4 A/m) or less.

39. The wiring board according to claim 32, wherein said magnetic loss material is selected from $Fe_\alpha-Al_\beta-O_\gamma$ and $Fe_\alpha-Si_\beta-O_\gamma$.